P U M P

## Pump basces.



The head or pressure that a pump will develop is in direct relation to the impeller diameter, the number of impellers, the eye or inlet opening size, and how much velocity is developed from the speed of the shaft rotation. Capacity is determined by the exit width of the impeller. All of these factors affect the horsepower size of the motor to be used; the more water to be pumped or pressure to be developed, the more energy is needed.
A centrifugal pump is not positive acting. As the depth to water increases, it pumps less and less water. Also, when it pumps against increasing pressure it pumps less water. For these reasons it is important to select a centrifugal pump that is designed to do a particular pumping job. For higher pressures or greater lifts, two or more impellers are commonly used; or, a jet ejector is added to assist the impellers in raising the pressure.

## Which Pump DonNeedP

The two most popular types used for private well systems or low flow irrigation applications are jet pumps and submersible pumps.

## JET PUMPS

Jet Pumps are mounted above ground and lift the water out of the ground through a suction pipe. Jets are popular in areas with high water tables and warmer climates. There are two categories of jet pumps and pump selection varies depending on water level. Shallow well installations go down to a water depth of about 25 feet. Deep wells are down 150 feet to water, where surface pumps are involved.

The jet pump is a centrifugal pump with one or more impeller and diffuser with the addition of a jet ejector. A JET EJECTOR consists of a matched nozzle and venturi. The nozzle receives water at high pressure. As the water passes through the jet, water speed (velocity) is greatly increased, but the pressure drops. This action is the same as the squirting action you get with a garden hose as when you start to close the nozzle. The greatly increased water speed plus the low pressure around the nozzle tip, is what causes suction to develop around the jet nozzle. Water around a jet nozzle is drawn into the water stream and carried along with it.

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UMP BASICS

Typical Jet Pump Installations


For a jet nozzle to be effective it must be combined with a venturi. The venturi changes the high-speed jet stream back to a high-pressure for delivery to the centrifugal pump. The jet and venturi are simple in appearance but they have to be well engineered and carefully matched to be efficient for various pumping conditions. The jet nozzle and venturi are also known as ejectors/ejector kits.

On a shallow-well jet pump the ejector kit (jet nozzle and venturi) is located in the pump housing in front of the impeller.

A portion of the suction water is recirculated through the ejector with the rest going to the pressure tank. With the ejector located on the suction side of the pump, the suction is increased considerably. This enables a centrifugal pump to increase its effective suction lift from about 20 feet to as much as 28 feet. But, the amount of water delivered to the storage tank becomes less as the distance from the pump to the water increases... more water has to be recirculated to operate the ejector.

The difference between a deep-well jet pump and a shallow-well jet pump is the location of the ejector. The deep-well ejector is located in the well below the water level. The deep-well ejector works in the same way as the shallow-well ejector. Water is supplied to it under pressure from the pump. The ejector then returns the water plus an additional supply from the well, to a level where the centrifugal pump can lift it the rest of the way by suction.

A convertible jet pump allows for shallowwell operation with the ejector mounted on the end of the pump body. This type of pump can be converted to a deep-well jet pump by installing the ejector below the water level.


How a jet provides pumping action
Water is supplied to the Jet ejector under pressure. Water surrounding the jet stream is lifted and carried up the pipe as a result of the jet action.
When a jet is used with a centrifugal pump a portion of the water delivered by the pump is returned to the jet ejector to operate It. The jet lifts water from the well to a level where the centrifugal pump can finish lifting It by suction. P U M P BASICS SIZING

This is of particular value when you have a water level that is gradually lowering. This will probably require a change of venturi to work efficiently.


## SUBMERSIBLE PUMPS

The submersible pump is a centrifugal pump. Because all stages of the pump end (wet end) and the motor are joined and submerged in the water, it has a great advantage over other centrifugal pumps. There is no need to recirculate or generate drive water as with jet pumps, therefore, most of its energy goes toward "pushing" the water rather than fighting gravity and atmospheric pressure to draw water.

Virtually all submersibles are "multi-stage" pumps. All of the impellers of the multi-stage submersible pump are mounted on a single shaft, and all rotate at the same speed. Each impeller passes the water to the eye of the next impeller through a diffuser. The diffuser is shaped to slow down the flow of water and convert velocity to pressure. Each impeller and matching diffuser is called a stage. As many stages are used as necessary to push the water out of the well at the required system pressure and capacity. Each time water is pumped from one impeller to the next, its pressure is increased.

The pump and motor assembly are lowered into the well by connecting piping to a position below the water level. In this way the pump is always filled with water (primed) and ready to pump. Because the motor and pump are under water they operate more quietly than above ground installations; and, pump freezing is not a concern.

We can stack as many impellers as we need; however, we are limited to the horsepower of the motor. We can have numerous pumps that have $1 / 2 \mathrm{HP}$ ratings - pumps that are capable of pumping different flows at different pumping levels; they will, however, always be limited to $1 / 2$ HP. Another way to look at it is that a pump will always operate somewhere along its design curve.


To get more flow, the exit width of the impeller is increased and there will then be less pressure (or head) that the pump will develop because there will be less impellers on a given HP size pump. Remember, the pump will always trade-off one for the other depending on the demand of the system. If the system demands more than a particular pump can produce, it will be necessary to go up in horsepower; thereby, allowing us to stack more impellers or go to different design pump with wider impellers.





A curve simply stated is normally a curved line drawn over a grid of vertical and horizontal lines. The curved line represents the performance of a given pump. The vertical and horizontal grid lines represent units of measure to display that performance.
Let's think of a well full of water. We want to use the water in a home. The home is at a higher level than the water in the well. Since gravity won't allow water to flow uphill, we use a pump. A pump is a machine used to move a volume of water a given distance. This volume is measured over a period of time expressed in gallons per minute (GPM) or gallons per hour (GPH).
The pump develops energy called discharge pressure or total dynamic head. This discharge pressure is expressed in units of measure called pounds per square inch (psi) or feet of head (ft).

NOTE: 1 psi will push a column of water up a pipe a distance of $2.31^{\prime}$. When measuring a pump's performance, we can use a curve to determine which pump is best to meet our requirements.

Figure 1 is a grid with the unit of measure in feet on the left hand side. We start with 0 at the bottom. The numbers printed as you go up the vertical axis relate to the ability of the pump to produce pressure expressed in feet. Always determine the value of each grid line. Sometimes the measure will say feet head, which is what most engineers call it.
With the pump running a reading was taken from the gauge in psi and converted to feet ( $1 \mathrm{psi}=2.31$ feet).

We show another unit of measure in gallons per minute across the bottom. You start with 0 on the left. The numbers printed as you go to the right relate to the ability of the pump to produce flow of water expressed as capacity-in gallons per minute (GPM). Again, always determine the value of each grid line.

To establish a pump curve we run the pump using a gauge, valve and flowmeter on the discharge pipe. We first run the pump with the valve closed and read the gauge. This gives us the pump's capability at 0 capacity and maximum head in feet.
Figure 2 - We mark the grid point 1. Next we open the valve to 8 GPM flow, for example, and read the gauge.
We again mark this point on the grid 2 . We continue this process until we have marked all the points on the grid.
Figure 3 - We now connect all the points. This curved line is called a head/capacity curve. Head $(\mathrm{H})$ is expressed in feet and capacity $(\mathrm{C})$ is expressed in gallons per minute (GPM). The pump will always run somewhere on the curve.

When the TDH is known, read vertically up the left hand side of the curve to that requirement, for example, 300 feet. Then read horizontally to a point on a curve that connects to the capacity needed, for example 26 GPM. It is then determined that a 3 HP 19 stage pump is needed.

There are many different type curves shown in our catalog. Figure 4 is a composite performance curve (more than one pump) for the submersible. There is a separate curve for each horsepower size. Let's compare two sizes:

1. First look at the $1 \mathrm{HP}, 8$ stages (impellers and diffusers). At 20 GPM capacity this model will make 160 feet.
2. Now look at the $5 \mathrm{HP}, 28$ stages. At 20 GPM capacity this model will make 500 feet.

When you add impellers, the pump makes more pressure (expressed in feet). This allows the pump to go deeper in a well, but also takes more horsepower.


## -Submersiblerumps

Well Size

## MORE ABOUT...

## VERTICAL LIFT/ ELEVATION

The vertical distance between the well head and the level at the point of use. It must be added to the TOTAL DYNAMIC HEAD if the inlet is lower than the outlet and subtracted if the inlet is higher. As a rule of good installation practice, however, pipes should slope continuously upward from the inlet to the outlet to prevent entrapment of air.

## SERVICE PRESSURE

The range of pressure in the pressure tank during the pumping cycle.

## PUMPING LEVEL

The lowest water level reached during pumping operation. (Static level - drawdown)

## STATIC OR STANDING WATER

 LEVELThe undisturbed level of water in the well before pumping. Not as important as pumping level.

## DRAWDOWN

The distance that the water level in the well is lowered by pumping. It is the difference between the STATIC WATER LEVEL and the PUMPING LEVEL.

## FRICTION LOSS

The loss of pressure or head due to the resistance to flow in the pipe and fittings. Friction loss is influenced by pipe size and fluid velocity, and is usually expressed in feet of head.

## HORIZONTAL RUN

The horizontal distance between the point where fluid enters a pipe and the point at which it leaves.

TOTAL DYNAMIC HEAD or TDH TDH and capacity required determines pump size. The total pressure or head the pump must develop is the sum of the VERTICAL LIFT/ELEVATION, THE SERVICE PRESSURE, PUMPING LEVEL, and THE FRICTION LOSS. All of these measurements must be expressed in the same units, usually feet of head or pressure (PSI), before adding them together.

## Determining Total Dynamic Head

## HEAD

## Vertical Lift / Elevation

The vertical distance in feet from the pitless adapter to the top of the pressure tank


- Service Pressure

The average (pump shut-off) pressure switch setting $\times 2.31^{\prime}$.
Example for a $30 / 50$ switch: $40 \times 2.31^{\prime}=92.4$ feet


## Pumping Level

ertical distance in feet from the pitless adapter or well seal to the water drawdown level in the well that yelds the flow rate required by the pump

## Friction Loss

Water flowing through piping will lose head depending on the size, type and length of piping, number of fittings, and flow rate. Example: Pumping 20 GPM through 500 ft . of 1 1/4" plastic pipe with three elbows will cause a friction loss equal to:
$\frac{500 \mathrm{ft} .+21 \mathrm{ft} . \text { (elbow loss) }}{100 \mathrm{ft} .} \times 6.00 \mathrm{ft}$ (loss per $100{ }^{\prime}$ ) $=31.26 \mathrm{ft}$.
Feet of Pipe $\qquad$ Diameter of Pipe $\qquad$
Type of Pipe $\qquad$
See Friction Loss Charts on Page 10

## Total Dynamic Head

After determining TDH, match this number with capacity required on pump curves of specific pumps in this catalog to select the correct pump.

Gallons Per Minute (or Hour) Needed

## Determining Flow Rate

Although methods will vary, in general, the Water Systems Council bases pump flow selection for a residential system on total gallon usage during a seven minute peak demand period. This can be supplemented by using a properly sized pressure tank.
Farms, irrigation and sprinkling demand more water.

## Typical Jet Pump Installations



## Aboveground Pumps

The difference between submersible pump and surface pump sizing is that surface pumps, including jet pumps, show performance in "charted" form versus "curves" for submersibles. Except for the "pumping level" (which is shown in feet in the charts) all other head/lift requirements should be converted to PSIG for surface pump sizing. (Feet X . $433=$ PSIG (Pounds per Square Inch Gage).

Well Size
(inside diameter in inches)

## MORE ABOUT...

VERTICAL LIFT/ ELEVATION
The vertical distance between the well head and the level at the point of use. It must be ADDED to the Total Dynamic/Total Discharge Head if the inlet is lower than the outlet and SUBTRACTED if the inlet is higher. As a rule of good installation practice, however, pipes should slope continuously upward from the inlet to the outlet to prevent entrapment of air.

## SERVICE PRESSURE

The range of pressure in the pressure tank during the pumping cycle.

## FRICTION LOSS

The loss of pressure or head due to the resistance to flow in the pipe and fittings. Friction loss is influenced by pipe size and fluid velocity, and is usually expressed in feet of head.

## HORIZONTAL RUN

The horizontal distance between the point where fluid enters a pipe and the point at which it leaves.

TOTAL DYNAMIC/TOTAL DIS-
CHARGE HEAD or TDH
TDH and capacity required determines pump size. The total pressure or head the pump must develop is the sum of Vertical Lift/ Elevation, The Service Pressure, and The Friction Loss. All of these measurements must be expressed in the same units, usually feet of head or pressure (PSI), before adding them together. For aboveground pumps, distance to water in feet are shown in the respective charts.

## PUMPING LEVEL

The lowest water level reached during pumping operation. (Static level minus drawdown)

## STATIC OR STANDING WATER

 LEVELThe undisturbed level of water in the well before pumping. Not as important as pumping level.

## DRAWDOWN

The distance that the water level in the well is lowered by pumping. It is the difference between the STATIC WATER LEVEL and the PUMPING LEVEL.

## Vertical Lift / Elevation

1 The vertical distance in feet from the location of the pump to the point of highest delivery (e.g. from a pump house near the well to the second floor of a two story house)

## Service Pressure

The average pressure switch setting.
Example 20/40 switch (1/2 HP) = 30 PSIG average ( $3 / 4 \mathrm{HP}$ and larger pumps have 30/50 switch settings) $=40$ PSIG average
 ing 10 GPM through 100 ft . of 1 " plastic pipe with 3 elbows will cause a friction loss equal to:
$\frac{100 \mathrm{ft} .+18 \mathrm{ft} . \text { (elbow loss) }}{100 \mathrm{ft} .} \mathrm{X} 6.31 \mathrm{ft}\left(\right.$ loss per $\left.100^{\prime}\right)=7.44^{\prime} \mathrm{X} .433=3.2 \mathrm{PSIG}$
Feet of Pipe $\qquad$ Diameter of Pipe $\qquad$
Type of Pipe $\qquad$
See Friction Loss Charts on Page 10

## 4. Total Dynamic/Discharge Head • $1+2+3=$

## Pumping Level/Depth to Water

The vertical distance in feet from the pump to the water level including draw down level - if any. In Shallow Well systems, referred to as suction lift/head and is limited to 20 or 25 feet at sea level (deduct 1' suction capability for each 1000' above sea level).


Note: Friction losses (3) in the suction piping must be added $\begin{array}{ll}\begin{array}{ll}\text { No need to } \\ \text { convert- } \\ \text { Charts are }\end{array} & \\ & \end{array}$ in feet

If 25' or less, use shallow well charts
to the pumping level for total suction lift.
If more than $\mathbf{2 5}^{\prime}$

Deep Well jet pump charts include the friction losses in the vertical piping only. See page15 if long horizontal, offset piping cannot be avoided.

## Determining Flow Rate

Although methods will vary, in general, the Water Systems Council bases pump flow selection for a residential system on total gallon usage during a seven minute peak demand period. This can be supplemented by using a properly sized pressure tank.

Farms, irrigation and sprinkling demand more water.
Gallons Per Minute (or hour) Needed
See Page 14 for water demands


After determining TDH and flow requirements in GPM / GPH, match these numbers with surface pump charts in sections 3 and 4.

## FictionLossCherts

Loss of head in feet, due to friction per 100 feet of pipe

| 3/4 Pipe |
| :---: | :---: | :---: |
| FLOW <br> US GAL <br> MIN STEEL <br> C--100 <br> ID.824" PLASTIC <br> ID-140 <br> ID <br> 1.5 1.13 .61 <br> 2.0 1.93 1.04 <br> 2.5 2.91 1.57 <br> 3.0 4.08 2.21 <br> 3.5 5.42 2.93 <br> 4.0 6.94 3.74 <br> 4.5 8.63 4.66 <br> 5.0 10.50 5.66 <br> 6.0 -- 7.95 <br> 7.0 -- 10.60 |


| " Pipe |  |  |
| :---: | :---: | :---: |
| FLOW <br> US GAL <br> MIN | STEEL <br> C-100 <br> ID.049" | PLASTIC <br> ID $1.049 "$ |
| 2 | .595 | .322 |
| 3 | 1.26 | .680 |
| 4 | 2.14 | 1.15 |
| 5 | 3.42 | 1.75 |
| 6 | 4.54 | 2.45 |
| 8 | 7.73 | 4.16 |
| 10 | 11.7 | 6.31 |
| 12 | -- | 8.85 |
| 14 | -- | 11.8 |

1 1/4" Pipe

| FLOW <br> US GAL <br> MIN | STEEL <br> C-100 <br> ID.380" | PLASTIC <br> C-140 <br> ID $1.380 "$ |
| :---: | :---: | :---: |
| 4 | .564 | .304 |
| 5 | .853 | .460 |
| 6 | 1.20 | .649 |
| 7 | 1.59 | .860 |
| 8 | 2.04 | 1.10 |
| 10 | 3.08 | 1.67 |
| 12 | 4.31 | 2.33 |
| 14 | 5.73 | 3.10 |
| 16 | 7.34 | 3.96 |
| 18 | 9.13 | 4.93 |
| 20 | 11.10 | 6.00 |
| 25 | -- | 9.06 |

$3^{3 \prime}$ Pipe

| FLOW <br> US GAL <br> MIN | STEEL <br> C-100 <br> ID 3.0" | PLASTIC <br> C-10 3068" |
| :---: | :---: | :---: |
| 20 | .149 | .129 |
| 30 | .316 | .267 |
| 40 | .541 | .449 |
| 50 | .825 | .676 |
| 60 | 1.17 | .912 |
| 70 | 1.57 | 1.22 |
| 80 | 2.03 | 1.56 |
| 90 | 2.55 | 1.95 |
| 100 | 3.12 | 2.37 |
| 110 | 3.75 | 2.84 |
| 120 | 4.45 | 3.35 |
| 130 | 5.19 | 3.90 |
| 140 | 6.00 | 4.50 |

1 1/2" Pipe

| FLOW <br> US GAL <br> MIN | STEEL <br> C-10 <br> ID 1.61" | PLASTIC <br> C-140 <br> ID 1.61" |
| :---: | :---: | :---: |
| 4 | .267 | .144 |
| 6 | .565 | .305 |
| 8 | .962 | .520 |
| 10 | 1.45 | .785 |
| 12 | 2.04 | 1.10 |
| 14 | 2.71 | 1.46 |
| 16 | 3.47 | 1.87 |
| 18 | 4.31 | 2.33 |
| 20 | 5.24 | 2.83 |
| 25 | 7.90 | 4.26 |
| 30 | 11.1 | 6.0 |
| 35 | -- | 7.94 |
| 40 | -- | 10.20 |


| FLOW <br> US GAL <br> MIN | STEEL <br> C-100 <br> ID 4.0" | PLASTIC <br> ID-140 $4.026 " ~$ |
| :---: | :---: | :---: |
| 20 | .038 | .035 |
| 30 | .076 | .072 |
| 40 | .128 | .120 |
| 50 | .194 | .179 |
| 60 | .273 | .250 |
| 70 | .365 | .330 |
| 80 | .470 | .422 |
| 90 | .588 | .523 |
| 100 | .719 | .613 |
| 110 | .862 | .732 |
| 120 | 1.02 | .861 |
| 130 | 1.19 | 1.00 |
| 140 | 1.37 | 1.15 |

Example:
10 GPM with 1 ' plastic pipe has 6.31 ' of loss per 100 ft . - if your run is 50 ft ., multiply by .5 , if 250 ft . multiply by 2.5 , etc.
Loss through fittings in terms of equivalent lengths of pipe

| TYPE FITTING \& APPLICATION | PIPE \& FTG MATERIAL. (Note 1) | EQUIVALENT LENGTH OF PIPE NOMINAL SIZE FITTING \& PIPE |  |  |  |  |  |  | TYPE FITTING \& APPLICATION | PIPE \& FTG. MATERIAL. (Note 1 | EQUIVALENT LENGTH OF PIPE NOMINAL SIZE FITTING \& PIPE |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 1/2 | 3/4 | 1 | 11/4 | 11/2 | 2 | 21/2 |  |  | 1/2 |  | 1 | 11/4 | 11/2 | 2 | $2^{1 / 2}$ |
| Insert coupling | Plastic | 3 | 3 | 3 | 3 | 3 | 3 | 3 | Standard tee Flow through side | Steel Copper Plastic | $\begin{aligned} & 4 \\ & 4 \\ & 7 \end{aligned}$ | $\begin{aligned} & 5 \\ & 5 \\ & 8 \\ & 8 \end{aligned}$ | $\begin{aligned} & 6 \\ & 6 \\ & 9 \end{aligned}$ | $\begin{gathered} 8 \\ 8 \\ 8 \\ 12 \end{gathered}$ | $\begin{array}{\|c} 9 \\ 9 \\ 13 \end{array}$ | $\begin{aligned} & 11 \\ & 11 \\ & 17 \end{aligned}$ | 14 <br> 14 <br> 20 |
| Threaded adapter |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Plastic or copper to thread | Copper Plastic | $\begin{aligned} & 1 \\ & 3 \end{aligned}$ | $\begin{aligned} & 1 \\ & 3 \end{aligned}$ | $\begin{aligned} & 1 \\ & 3 \end{aligned}$ | $\begin{aligned} & 1 \\ & 3 \end{aligned}$ | $\begin{aligned} & 1 \\ & 3 \end{aligned}$ | $\begin{aligned} & 1 \\ & 3 \end{aligned}$ | $\begin{array}{\|l\|} 1 \\ 3 \end{array}$ | Gate valve | Note 2 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| $90^{\circ}$ standard elbow | Steel | 2 | 3 | 3 | 4 | 4 |  |  | Swing check valve | Note 2 | 4 | 5 | 7 | 9 | 11 | 13 | 16 |
|  | Copper | 2 | 3 | 3 | 4 | 4 | 5 | 6 |  |  |  |  |  |  |  |  |  |
|  | Plastic | 4 | 5 | 6 | 7 | 8 | - | 10 |  |  |  |  |  |  |  |  |  |

Note 1: Loss figures are based on equivalent lengths of indicated pipe material
Note 2: Loss figures are for screwed valves and are based on equivalent lengths of steel pipe
-Loss figures for copper lines are approximately $10 \%$ higher than shown for plastic

## Pressure-Ianksizing



## Why do I need a tank?

There are four main reasons to include a tank in your system:

1. To protect and extend the life of the pump by reducing the number of cycles.
2. To provide storage of water under pressure for delivery between cycles.
3. To have reserve capacity for periods of peak demand.
4. To reduce system maintenance.

## How do I choose a tank for my system?

Choosing the proper tank for your pumping system will greatly reduce the risk of premature pump failure. Most manufacturers recommend a minimum run time of one minute in order to protect the pump and the pump motor. The larger the tank the longer the running time and fewer pump cycles will result in longer pump life. 1 HP and larger pumps require longer run times.
To determine the proper size of tank, there are three factors to consider:

1. Pump flow rate in gallons per minute
2. Desired run time of the pump
3. Cut-in and cut-out psi of the pressure switch

From these factors you can determine the tank drawdown with the following equation:
Pump flow rate X run time = tank drawdown capacity required.
Tank drawdown capacity is the minimum amount of water stored and/or delivered by the pressure tank between pump shut-off and pump re-start. This should not be confused with "tank volume." For example, a pre-charged tank with a tank volume of 20 gallons has only 5 to 7 gallons drawdown capacity depending on the cut-in / cut-out (on/off) setting of the pressure switch.
Pumps with flow rates (capacities) up to 10 GPM should have a tank with a minimum of 1 gallon drawdown capacity for each GPM delivered by the pump. Example: 10 GPM pump = 10 gal. "drawdown"
Pump flow rates from 11 to 20 GPM should have tank drawdowns approximately 1.5 times the GPM rating. For example, 20 GPM X 1.5 = 30 gal. "drawdown"
Pump flow rates above 20 GPM should have tank drawdowns approximately 2 times the GPM rating and multiple tanks should be considered.
(Check your tank manufacturer's charts for tank drawdown rating.) Dinta

## Glossary

ACIDITY - A condition of water when the pH is below 7 . See pH .
ALKALINITY - A condition of water when the pH is above 7. See pH .
AQUIFER-A water-saturated geologic unit or system that yields water to wells or springs at a sufficient rate that the wells or springs can serve as practical sources of water.
ARTESIAN WELL (flowing and non-flowing) - Well where the water rises above the surface of the water in the aquifer after drilling is completed. It is a flowing artesian well if the water rises above the surface of the earth.
CENTRIFUGAL - consists of a fan-shaped impeller rotating in a circular housing, pushing liquid towards a discharge opening. Simple design, only wearing parts are the shaft seal and bearings (if so equipped). Usually used where a flow of liquid at relatively low pressure is desired. Not self-priming unless provided with a priming reservoir or foot valve: works best with the liquid source higher than the pump (flooded suction/gravity feed). As the discharge pressure (head) increases, flow and driven power requirements decrease. Maximum flow and motor loading occur at minimum head.

CHECK VALVE-Allows liquid to flow in one direction only. Generally used in suction and discharge line to prevent reverse flow.
CISTERN-A non-pressurized tank (usually underground) for storing water.
COAGULATION - The chemically combining of small particles suspended in water.
CONTAMINATED WATER—Water that contains a disease causing or toxic substances.
DEEP WELL - Use a pump (submersible or deep well jet) to force water upward from a pumping element below the well water level. Not restricted by suction lift limitations.
DRAWDOWN-The vertical distance the water level drops in a well pumped at a given rate.
DYNAMIC HEAD - Vertical distances (in feet) when the pump is running/producing water.
FLOODED SUCTION—Liquid source is higher than pump and liquid flows to pump by gravity. (Preferable for centrifugal pump installations.)

FLOW - The measure of the liquid volume capacity of a pump. Given in Gallons Per Hour (GPH) or Gallons Per Minute (GPM), as well as Cubic Meters Per Hour (CMPH), and Liters Per Minute (LPM).
FOOT VALVE-A type of check valve with a built-in strainer. Used at point of liquid intake to retain liquid in the system, preventing loss of prime when liquid source is lower than pump.
FRICTION LOSS - The loss of pressure or head due to the resistance to flow in the pipe and fittings. Friction loss is influenced by pipe size and fluid velocity, and is usually expressed in feet of head.
GRAINS PER GALLON-The weight of a substance, in grains, in a gallon. Commonly, grains of minerals per gallon of water as a measure of water hardness. $1 \mathrm{gpg}=17.1 \mathrm{mgl}$.
GROUND WATER-Water that has filtered down to a saturated geologic formation beneath the earth's surface.
HARDNESS MINERALS—Minerals dissolved in water that increase the scaling properties and decrease cleansing action - usually calcium, iron and magnesium.
HEAD-Another measure of pressure, expressed in feet. Indicates the height of a column of water being lifted by the pump neglecting friction losses in piping.
INCRUSTATION-A mineral scale chemically or physically deposited on wetted surfaces, such as well screens, gravel packs, and in tea kettles.
INTERMEDIATE STORAGE-A holding tank included in a water system when the water source does not supply the peak use rate.

JET PUMP - A pump combining two pumping principles - centrifugal operation and ejection. Can be used in shallow or deep wells.

MILLIGRAMS PER LITER (mg/l) - The weight of a substance, in milligrams in a liter. $1 \mathrm{mg} / \mathrm{l}=1 \mathrm{oz}$. per 7500 gallons. It is equivalent to 1 ppm ; see Parts per Million.
NEUTRALITY-A condition of water when the pH is at 7 . See pH .
OXIDATION-A chemical reaction between a substance and oxygen.
PALATABLE WATER - Water of acceptable taste. May also include non-offensive appearance and odor.
PARTS PER MILLION, ppm - A measure of concentration; one unit of weight or volume of one material dispersed in one million units of another; e.g., chlorine in water, carbon monoxide in air. Equivalents to indicate small size of this unit: $1 \mathrm{ppm}=1 \mathrm{oz}$. per 7500 gallons; 1 kernel of corn in 13 bushels $1 / 4 \mathrm{sq}$. in. in an acre.
PEAK USE RATE-The flow rate necessary to meet the expected maximum water demand in the system.
$\mathrm{pH}-\mathrm{A}$ measure of the acidity or alkalinity of water. Below 7 is acid, above 7 is alkaline.
POLLUTED WATER-Water containing a natural or man-made impurity.
POTABLE WATER-Water safe for drinking.
PRESSURE-The force exerted on the walls of a container (tank pipe, etc.) by the liquid. Measured in pounds per square inch (PSI).
PRIME-A charge of liquid required to begin pumping action of centrifugal pumps when liquid source is lower than pump. May be held in pump by a foot valve on the intake line or a valve or chamber within the pump.
RELIEF VALVE-Usually used at the discharge of a pump. An adjustable, spring-loaded valve opens, or relieves pressure when a pre-set pressure is reached. Used to prevent excessive pressure and pump or motor damage if discharge line is closed off.
SHALLOW WELL - Use a pump located above ground to lift water out of the ground through a suction pipe. Limit is a lift of 33.9 feet at sea level.
SOFTENING-The process of removing hardness caused by calcium and magnesium minerals.
SPRING-A place on the earth's surface where ground water emerges naturally.
STATIC HEAD-Vertical Distance (in Feet) from pump to point of discharge when the pump is not running.
STRAINERS - A device installed in the inlet of a pump to prevent foreign particles from damaging the internal parts.
SUBMERGENCE / SETTING - The vertical distance between PUMPING LEVEL and the bottom of the pump or jet assembly. Submergence must be sufficient to insure that the suction opening of the pump or jet assembly is always covered with water, while maintaining enough clearance from the bottom of the well to keep it out of sediment (at least 10 feet clearance is recommended). Could be useful when figuring friction loss.
SUBMERSIBLE-A pump which is designed to operate totally submersed in the fluid which is being pumped. With water-proof electrical connections, using a motor which is cooled by the liquid.
SUMP-A well or pit in which liquids collect below floor level.
SURGING-Forcing water back and forth rapidly and with more than normal force in a well or other part of the water system.
TOTAL HEAD-The sum of discharge head suction lift and friction losses.
VISCOSITY - The thickness of a liquid, or its ability to flow. Temperature must be stated when specifying viscosity, since most liquids flow more easily as they get warmer. The more viscous the liquid the slower the pump speed required.
WATER TABLE WELL-A well where the water level is at the surface of the aquifer.
WATER TREATMENT-A process to improve the quality of water.
WATER WELL-A man-made hole in the earth from which ground water is removed.
WELL DEVELOPMENT - A process to increase or maintain the yield of a well.

PUMP

## Metric Conversion Tables

## MEASUREMENT CONVERSION FACTORS (Approximate)




|  |  |
| :---: | :---: |
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## Centrifugal Pumps • Formulas a Conversion Factors



Lbs. per square in. = Head in ft. x . 433
Head in ft. = lbs. per sq. in. $\times 2.31$ '


## Ofiset let Pump

## Pipe Friction

Where the jet pump is offset horizontally from the well site, add the following distances to the vertical lift to approximate capacity to be received.

Friction loss in feet per 100 feet offset • Friction loss is to be added to vertical lift

| JET SIZE HP | 1114. $\times 1$ | $11 / 4 \times 11 / 4$ | $11 / 2 \times 11 / 4$ | $11 / 2 \times 11 / 2$ | $2 \times 11 / 2$ | $2 \times 2$ | 21/2x 2 | 21⁄2 $\times 21 / 2$ | $3 \times 21 / 2$ | $3 \times 3$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1/3 | 12 | 8 | 6 | 4 |  |  |  |  |  |  |
| 1/2 | 18 | 12 | 8 | 6 | 3 | 2 |  |  |  |  |
| 3/4 | 30 | 22 | 16 | 11 | 6 | 4 |  |  |  |  |
| 1 |  | 30 | 25 | 16 | 9 | 6 |  |  |  |  |
| $11 / 2$ |  |  |  |  | 13 | 8 | 5 | 3 |  |  |
| 2 |  |  |  |  | 20 | 13 | 7 | 5 |  |  |
| 3 |  |  |  |  |  |  | 13 | 9 | 6 | 4 |

Example: Vertical distance to water is 60 feet, but a 100' horizontal / offset (run of piping) is required. A $3 / 4 \mathrm{HP}$ jet pump is used so the capacity should be taken from the " 80 ' depth to water" performance.

For example: 60' to water $+22^{\prime}$ Friction loss (with $11 / 4 \times 11 / 4$ two pipe system) $=82^{\prime}$, which is approximately 80'.

## Installation of a Long Tail Pipe on Deep Well Jet Pumps

The pumping capacity of a deep well jet pump can be reduced to equalize with the well flow by installing a 35 foot tail pipe below the jet assembly.
With a tail pipe, pump delivery remains at $100 \%$ of capacity down to the ejector level. If water level falls below that, flow decreases in proportion to drawdown as shown by figures. When delivery equals well inflow, the water level remains constant until the pump shuts off. The pump will not lose prime with this tail pipe arrangement.


## Drop cables election Chert

| 능 | Motor Rating |  |  | Copper Wire Size |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\bigcirc{ }^{\circ}$ | Volts | HP | KW | 14 | 12 | 10 | 8 | 6 | 4 | 3 | 2 | 1 | 0 | 00 | 000 | 0000 |
| § 山 | 115 | 1／2 | ． 37 | 100 | 160 | 250 | 390 | 620 | 960 | 1190 | 1460 | 1780 | 2160 | 2630 | 3140 | 3770 |
| $F \cdots$ |  | 1／2 | ． 37 | 400 | 650 | 1020 | 1610 | 2510 | 3880 | 4810 | 5880 | 7170 | 8720 |  |  |  |
| 山 山 |  | 3／4 | ． 55 | 300 | 480 | 760 | 1200 | 1870 | 2890 | 3580 | 4370 | 5330 | 6470 | 7870 |  |  |
| ¢ 之 |  | 1 | 75 | 250 | 400 | 630 | 990 | 1540 | 2380 | 2960 | 3610 | 4410 | 5360 | 6520 |  |  |
|  | 230 | 1.5 | 1.1 | 190 | 310 | 480 | 770 | 1200 | 1870 | 2320 | 2850 | 3500 | 4280 | 5240 |  |  |
|  |  | 2 | 1.5 | 150 | 250 | 390 | 620 | 970 | 1530 | 1910 | 2360 | 2930 | 3620 | 4480 |  |  |
| 山 \＃ |  | 3 | 2.2 | 120＊ | 190 | 300 | 470 | 750 | 1190 | 1490 | 1850 | 2320 | 2890 | 3610 |  |  |
|  |  | 5 | 3.7 | 0 | 0 | 180＊ | 280 | 450 | 710 | 890 | 1110 | 1390 | 1740 | 2170 | 2680 |  |
|  |  | 7.5 | 5.5 | 0 | 0 | 0 | 200＊ | 310 | 490 | 610 | 750 | 930 | 1140 | 1410 | 1720 |  |
| ○三 |  |  | 7.5 | 0 | 0 | 0 | 0 | 250＊ | 390 | 490 | 600 | 750 | 930 | 1160 | 1430 | 1760 |
| $\underset{\sim}{\square}$ |  | 15 | 11 | 0 | 0 | 0 | 0 | 170＊ | 270＊ | 340 | 430 | 530 | 660 | 820 | 1020 | 1260 |


|  | Motor Rating |  | Copper Wire Size（1） |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Volts | HP KW | 14 | 12 | 10 | 8 | 6 | 4 | 3 | 2 | 1 | 0 | 00 | 000 | 0000 |
|  |  | 1／2 ． 37 | 710 | 1140 | 1800 | 2840 | 4420 |  |  |  |  |  |  |  |  |
|  |  | $\begin{array}{cc}3 / 4 & .55\end{array}$ | 510 | 810 | 1280 | 2030 | 3160 |  |  |  |  |  |  |  |  |
|  | 200V | 1.75 | 430 | 690 | 1080 | 1710 | 2670 | 4140 | 5140 |  |  |  |  |  |  |
|  | 60 Hz | $\begin{array}{ll}1.5 & 1.1\end{array}$ | 310 | 500 | 790 | 1260 | 1960 | 3050 | 3780 |  |  |  |  |  |  |
|  |  | 21.5 | 240 | 390 | 610 | 970 | 1520 | 2360 | 2940 | 3610 | 4430 | 5420 |  |  |  |
|  | Three | 32.2 | 180 | 290 | 470 | 740 | 1160 | 1810 | 2250 | 2760 | 3390 | 4130 |  |  |  |
| $\boldsymbol{\omega}$ | Phase | $\begin{array}{ll}5 & 3.7\end{array}$ | 110＊ | 170 | 280 | 440 | 690 | 1080 | 1350 | 1660 | 2040 | 2490 | 3050 | 3670 | 4440 |
| 1 |  | 7.5 5.5 <br> 10 7.5 | 0 | 0 | 200 | 310 | 490 | 770 | 960 | 1180 | 1450 | 1770 | 2170 | 2600 | 3150 |
| $\bigcirc$ | Three | 107.5 | 0 | 0 | 0 | 230＊ | 370 | 570 | 720 | 880 | 1090 | 1330 | 1640 | 1970 | 2390 |
| $>$ | Wire | $15 \quad 11$ | 0 | 0 | 0 | 160＊ | 250＊ | 390 | 490 | 600 | 740 | 910 | 1110 | 1340 | 1630 |
| $\bigcirc$ |  | $20 \quad 15$ | 0 | 0 | 0 | 0 | 190＊ | 300＊ | 380 | 460 | 570 | 700 | 860 | 1050 | 1270 |
| ヘ |  | $\begin{array}{ll}25 & 18.5\end{array}$ | 0 | 0 | 0 | 0 | 0 | 240＊ | 300＊ | 370＊ | 460 | 570 | 700 | 840 | 1030 |
| 0 |  | $30 \quad 22$ | 0 | 0 | 0 | 0 | 0 | 0 | 250＊ | 310＊ | 380＊ | 470 | 580 | 700 | 850 |
| 2 |  | 1／2 ． 37 | 930 | 1490 | 2350 | 3700 | 5760 | 8910 |  |  |  |  |  |  |  |
| $\stackrel{\pi}{\mathbb{4}}$ |  | 3／4 ． 55 | 670 | 1080 | 1700 | 2580 | 4190 | 6490 | 8060 | 9860 |  |  |  |  |  |
| $0$ | 230V | 1.75 | 560 | 910 | 1430 | 2260 | 3520 | 5460 | 6780 | 8290 |  |  |  |  |  |
| N | 60 Hz | 1.51 .1 | 420 | 670 | 1060 | 1670 | 2610 | 4050 | 5030 | 6160 | 7530 | 9170 |  |  |  |
|  |  | 21.5 | 320 | 510 | 810 | 1280 | 2010 | 3130 | 3890 | 4770 | 5860 | 7170 | 8780 |  |  |
|  | Three | 32.2 | 240 | 390 | 620 | 990 | 1540 | 2400 | 2980 | 3660 | 4480 | 5470 | 6690 | 8020 | 9680 |
|  | Phase | 53.7 | 140＊ | 230 | 370 | 590 | 920 | 1430 | 1790 | 2190 | 2690 | 3290 | 4030 | 4850 | 5870 |
| 山ீШ |  | 7.5 5.5 <br> 10 7.5 | 0 | 160＊ | 260 | 420 | 650 | 1020 | 1270 | 1560 | 1920 | 2340 | 2870 | 3440 | 4160 |
| $\cdots$ | Three | 107.5 | 0 | 0 | 190＊ | 310 | 490 | 760 | 950 | 1170 | 1440 | 1760 | 2160 | 2610 | 3160 |
|  | Wire | 1511 | 0 | 0 | 0 | 210＊ | 330 | 520 | 650 | 800 | 980 | 1200 | 1470 | 1780 | 2150 |
|  |  | $20 \quad 15$ | 0 | 0 | 0 | 0 | 250＊ | 400 | 500 | 610 | 760 | 930 | 1140 | 1380 | 1680 |
| 山三 |  | $\begin{array}{ll}25 & 18.5\end{array}$ | 0 | 0 | 0 | 0 | 0 | 320＊ | 400 | 500 | 610 | 750 | 920 | 1120 | 1360 |
| $\underset{\sim}{\underline{E}}$ |  | $30 \quad 22$ | 0 | 0 | 0 | 0 | 0 | 260＊ | 330＊ | 410＊ | 510 | 620 | 760 | 930 | 1130 |
| § ш |  | 1／2 ． 37 | 3770 | 6020 | 9460 |  |  |  |  |  |  |  |  |  |  |
| Ш |  | 3／4 ． 55 | 2730 | 4350 | 6850 |  |  |  |  |  |  |  |  |  |  |
| $\ddot{\sim}$ |  | 1.75 | 2300 | 3670 | 5770 | 9070 |  |  |  |  |  |  |  |  |  |
| $\underset{\sim}{x}$ |  | 1.51 .1 | 1700 | 2710 | 4270 | 6730 |  |  |  |  |  |  |  |  |  |
|  |  | 21.5 | 1300 | 2070 | 3270 | 5150 | 8050 |  |  |  |  |  |  |  |  |
| Ш゙ | 460v | 32.2 | 1000 | 1600 | 2520 | 3970 | 6200 |  |  |  |  |  |  |  |  |
| $\boldsymbol{\sim}$ | 60 Hz | $\begin{array}{ll}5 & 3.7\end{array}$ | 590 | 950 | 1500 | 2360 | 3700 | 5750 |  |  |  |  |  |  |  |
| 4 |  | $\begin{array}{ll}7.5 & 5.5\end{array}$ | 420 | 680 | 1070 | 1690 | 2640 | 4100 | 5100 | 6260 | 7680 |  |  |  |  |
| －1 | Three | 107.5 | 310 | 500 | 790 | 1250 | 1960 | 3050 | 3800 | 4680 | 5750 | 7050 |  |  |  |
| 山 | Phase | $15 \quad 11$ | 0 | 340＊ | 540 | 850 | 1340 | 2090 | 2600 | 3200 | 3930 | 4810 | 5900 | 7110 |  |
| Ш |  | $20 \quad 15$ | 0 | 0 | 410＊ | 650 | 1030 | 1610 | 2000 | 2470 | 3040 | 3730 | 4580 | 5530 |  |
| $\underset{\sim}{\boldsymbol{\sim}}$ | Three | $\begin{array}{ll}25 & 18.5\end{array}$ | 0 | 0 | 0 | 530＊ | 830 | 1300 | 1620 | 1990 | 2450 | 3010 | 3700 | 4470 | 5430 |
| ト | Wire | 3022 | 0 | 0 | 0 | 430＊ | 680 | 1070 | 1330 | 1640 | 2030 | 2490 | 3060 | 3700 | 4500 |
|  |  | 4030 | 0 | 0 | 0 | 0 | 500＊ | 790 | 980 | 1210 | 1490 | 1830 | 2250 | 2710 | 3290 |
|  |  | $50 \quad 37$ | 0 | 0 | 0 | 0 | 0 | 640＊ | 800 | 980 | 1210 | 1480 | 1810 | 2190 | 2650 |
|  |  | $60 \quad 45$ | 0 | 0 | 0 | 0 | 0 | 540＊ | 670＊ | 830＊ | 1020 | 1250 | 1540 | 1850 | 2240 |
|  |  | 7555 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 680＊ | 840＊ | 1030 | 1260 | 1520 | 1850 |
|  |  | 10075 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 620＊ | 760＊ | 940＊ | 1130 | 1380 |
|  |  | 12590 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 740＊ | 890＊ | 1000＊ |
|  |  | 150 110 <br> 175 130 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 760＊ | 920＊ |
|  |  | 175130 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 810＊ |
|  |  | 200150 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

Lengths marked $*$ meet the U．S．National Electrical Code ampacity only for individual conductor $75^{\circ} \mathrm{C}$ ．cable．Only the lengths without $\star$ meet the code for jacketed $75^{\circ} \mathrm{C}$ cable．Local code requirements may vary．
CAUTION！！Use of wire sizes smaller than determined above will void warranty，since low starting voltage and early failure of the unit will result．Larger wire sizes （smaller numbers）may always be used to improve economy of operation．
（1）If aluminum conductor is used，multiply above lengths by 0.61 ．Maximum allowable length of aluminum wire is considerably shorter than copper wire of same size．

