Rail Dynamics Laboratory

Performance Requirements & Hardware Configurations

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ABSTRACT

This paper describes the Rail Dynamics Laboratory (RDL) facility at the Transportation Test Center (TTC), Pueblo, Colorado. Two unique test machines, the Vibration Test Unit (VTU) and the Roll Dynamics Unit (RDU) are to be housed in this facility to perform dynamic tests of full-scale rail-road and transit industry vehicles. Both the VTU and RDU performance requirements and hardware configurations are described.

INTRODUCTION

The objectives of this paper are to acquaint the reader with the Rail Dynamics Laboratory (RDL) facility at the Transportation Test Center (TTC), Pueblo, Colorado; and to review the performance requirements and hardware configurations of two unique test machines that the RDL will house: the Vibration Test Unit (VTU) and the Roll Dynamics Unit (RDU).

The railroad and transit industries have frequently encountered dynamic operating problems with their vehicles leading to: injuries and fatalities, accidents and derailments, lading damage, excessive maintenance costs, and rough train rides for passengers. The Federal Railroad Administration (FRA) since the inception of TTC has long recognized the need for a rail dynamics laboratory as a research tool to conduct fundamental research in a controlled environment on the many dynamic factors affecting vehicle performance and safety. While the RDL facility is not fully operational as of yet, the goals and objectives through the years of development have remained relatively the same.

The RDL goal is to provide a facility to perform dynamic tests of full-scale locomotive, passenger and freight cars, transit vehicles and advanced track systems under controlled conditions. Such a facility will permit the evaluation of various hardware designs in a safe, controlled and reproducible scientific laboratory environment, allowing the performance of a variety of tests with minimal risk to personnel and equipment.

The objectives of the FRA RDL program for the past several years have been to provide an operational facility as soon as possible within reasonable costs that can be utilized by railroad and transit industry researchers in dynamic studies such as: passive and active suspension characteristics; vehicle rock and roll tendencies; component stress analysis; component and vehicle natural frequencies; adhesions; ride comfort; acceleration; braking; lading responses; hunting and analytical model validation as well as supporting causes of derailment. This facility will help to isolate the causes of and aid in the solutions to various dynamic operating problems encountered in the railroad and transit industry. Through study of vehicle dynamics in the RDL, the number of dynamic-related accidents and derailments and their attendant costs should be reduced significantly.

RDL HISTORY

Todays RDL facility is considerably different than what was originally planned at the inception of the program at FRA many years earlier, as will be explained. Prior to the development of DOT's TTC, no test facility was available in the United States to extensively evaluate and determine the solutions to dynamic operation problems. Just before 1970, FRA contractor studies recommended a full-scale roller rig (a rail dynamics simulator) with capability to handle cars and locomotives at full speed and power, with vibrations applied through the wheels to simulate track conditions. Representation of railroads and suppliers assisted FRA in preparing performance specifications for the simulator.

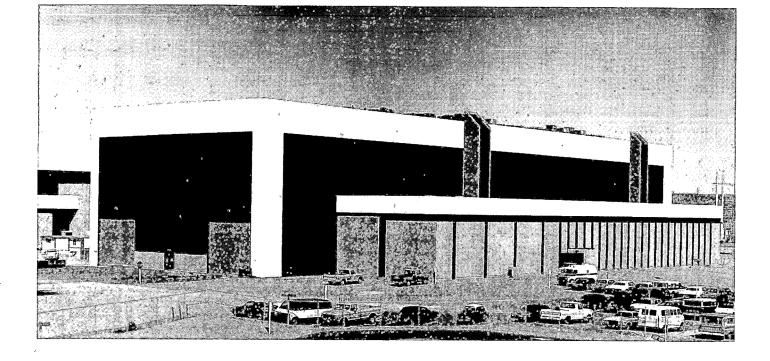


Fig. 1, Rail Dynamics Laboratory Building

FRA engineers opened communications with experts in other countries who had operated similar facilities to use their experience in preparation of the specifications. In order to leave options open for testing advanced high speed systems, such as the tracked air cushion vehicles, the simulator speed capability was designed for approximately 300 mph (483 km/h). The Urban Mass Transportation Administration joined in funding part of the RDL project so that transit vehicles could also be tested in the laboratory and agreed with FRA to locate the rail dynamics simulator (RDS) in a laboratory at TTC.

RDL Building

FRA placed the RDL building construction contract in 1972 for a high bay (the testing area) and a connecting low bay office wing, a two-story structure which contains offices, control room and other facility support areas. The principal dimensions of the high bay is 352' x 108' x 65' (107.3m x 32.9m x 19.8m) while the low bay is 264' x 50' x 30' (80.5m x 15.2m x 9.1m).

This modern steel and reinforced-concrete structure RDL building (Figure 1) was accepted in April 1974. Some notable features of the RDL building include: a) two high bay 100 ton overhead cranes for loading and off loading the test machines, b) calibration laboratory for instrumentation, c) electronic shop for equipment repairs and maintenance, d) clean rooms for disassembly, inspection and cleaning equipment.

Rail Dynamics Simulator (RDS) and Subsystems

The high bay portion of the RDL building was to house the RDS as well as service areas

and a vertical shaker. Starting in 1972, FRA let contracts for the following subsystems comprising the RDS:

a. Drive train, which was to provide rotation to the track module rollers;

b. Track module, which was to simulate the tracks on which the test vehicle rests and had the capability to simulate vertical and lateral irregularities;

c. Carriage assembly, which acted as the support and reaction structure for the track module;

d. Instrumentation and control subsystem.

- e. Computer subsystem.
- f. Communication system.

A separate contractor was involved with each subsystem.

Vertical Shaker System (VSS).

While the RDS subsystem was in the design phase, FRA awarded a contract to Wyle Laboratories to design and construct a Component/Vehicle Preliminary Evaluation System, later named the Vertical Shaker System (VSS), envisioned as a pre-test tool prior to complex testing on the RDS. The VSS was to be used for the determination of rough estimates of response modes and frequencies and for studying the responses of truck assemblies and total vehicles to vertically applied periodic excitation. In 1975, the VSS (Figure 2) was activated, it essentially consists of four independently operated vertical actuators which can be placed under four wheels of a two axle truck on one end of a rail vehicle. Each actuator can accommodate wheel loads of up to 40,000 pounds (18, 144 kg). The acceleration, frequency, and displacement of these actuators can be varied over a wide operating range to simulate operating environments of most test specimens.

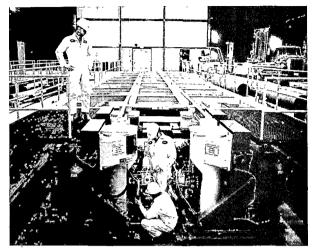


Fig. 2, Vertical Shaker System

Input capabilities for this system include: a) vertical translation of the truck and railcar, b) roll motion of the truck and railcar and c) pitch motion between the forward and aft axle sets. Prior to changes in the RDL program that affected the VSS configuration, two test programs were conducted in the RDL on the VSS:

(a) The Trailer-on-Flatcar (TOFC) Optimization Program (see Figure 3) which was designed primarily to determine the sensitivity of lading response to suspension system component variations and load distribution; and (b) the AAR Structural Dynamics evaluation of the TOFC configuration which was structured to collect data for verification of a mathematical model of the flat car body.

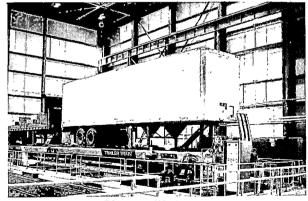


Fig. 3, TOFC on VSS

RDL Program Redirection

During the development of some of the RDS subsystems, unforeseen technical problems arose which resulted in severe schedule delays and associated risks of great concern to DOT.

In mid-1975, after the RDL program had con-

tinued to encounter R&D development and management problems, a DOT task force review resulted in the redirection of the RDL program so that it could be completed in a timely manner, relatively free of technical risk, and with minimum cost. The RDS was replaced by the Vibration Test Unit (VTU), on upgraded VSS, which will provide vertical and lateral excitation at both ends of a test vehicle, and the Roll Dynamics Unit (RDU), a basic roller rig. The RDS formerly combined both vibration and roll in one simulator. The redirected RDL program now has one prime contractor, Wyle Laboratories, instead of several major contractors.

The subsystems and systems which formerly supported the RDS, now as Government Furnished Property (GFP), will be modified for VTU and/or RDU operation, wherever possible. These subsystems/systems included the VSS, drive trains, hydraulic subsystem, integrated computer subsystem network, analog acquisition and control subsystem, and communication system, and structures subsystems. The RDL building floor plan including the VTU and RDU test pits is shown in Figure 4.

VTU DEFINITION/BASIC REQUIREMENT

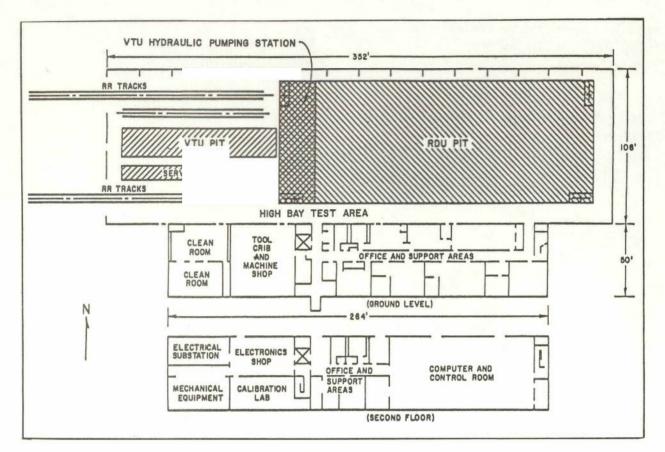
The VTU shall provide the capability for subjecting a 320,000 pound (145,150 kg) rail vehicle equipped with two, two-axle trucks or to one truck of a vehicle having three or four axles per truck, to the vertical and lateral vibrations environments which the vehicle and its components would "see" in traveling over track with representative profile and alignment variations.

RDU DEFINITION/BASIC REQUIREMENT

The RDU will provide the capability for driving, or absorbing power from the wheel sets of a four-axle vehicle or a three or four axle locomotive truck. One roller module shall be provided for each wheel set. Through rotation of the rollers, the RDU will simulate tangent track at various vehicle velocities, and will permit investigation of dynamic phenomena characteristics of "perfect" tangent track such as truck hunting. "Perfect" track is defined as track with no lateral or vertical irregularities.

VTU PERFORMANCE REQUIREMENTS

A brief summary of the major VTU performance requirements are noted here. Table 1 identifies the test vehicle weight and size limitations for VTU. The VSS vertical actuators (as GFP) was the primary factor for the maximum vehicle weight requirements.







90.0 ft (27.43m) 108.0 ft (32.92m) Vehicle Length (max) Vehicle Width (max) 12.0 ft (3.66m) 12.0 ft (3.66m) Vehicle Weight (max) 320,000 lb 400,000 lb (181,437 kg) (145,150 kg) Axle Load (max) 80,000 lb 100,000 1b (45,360 kg) (36,287 kg) 20.0 ft (6.10m) 70.0 ft (21.34m) Truck Center Distance (min) 20.0 ft (6.10m) (max) 80.0 ft (24.38 kg) 54.0 in. (1.37m) Truck Axle Spacing (min) 54.0 in. (1.37m) (max) 110.0 in. (2.79m) 110.0 in. (2.79m) 56.5 in. (1.44m) 66.0 in. (1.68m) 56.5 in. (1.44m) 66.0 in. (1.68m) Gauge (min) (max) Coupler Centerline to Railhead 17.5 in. (0.44m) 34.5 in. (0.88m) 17.5 in. (0.44m) 34.5 in. (0.88m) (min) (max) Center of Gravity to Railroad 18.0 in. (0.46m) 98.0 in. (2.49m) (min) 18.0 in. (0.46m) (max) 98.0 in. (2.49m)

The Table 2 summarizes the vertical and lateral excitation motion requirements.

Table 2. VTU Vertical and Lateral Excitation

	Excita	tion
	<u>Vertical</u>	<u>Lateral</u>
Frequency Range	0.2 to 30 Hz	0.2 to 30 Hz
Displacement	+ 2"(5.08cm)	⁺ 1.5"(3.81cm)
Velocity	25 inch/sec. (63.5 cm/sec)	15 inch/sec. (38.1 cm/sec)
Acceleration	3.5 q's	3.1 a's

The VTU is to provide the following types of vibratory motions to the test vehicle: vertical translation, pitch motions, roll motions, lateral translation, yaw motions, time delayed motions, combined rigid body motions, combined time delay motions and arbitrary wheel vibrations. These modes of vibration are shown in Figure 5. vehicle or causing any hazard to operating/maintenance personnel.

VTU HARDWARE CONFIGURATION

As previously identified the VTU hardware had to be designed to provide the capability to subject a variety of rail vehicles to vertical and lateral vibratory environments similar to that experienced during over-the-road operations.

Owing to the variety of vehicle configurations to be accommodated, each with a unique set of dimensions associated with such elements as axle spacing, truck center distance, overhang, coupler height (in the case of transit vehicle) and inertial properties a modular approach to hardware implementation was required. In addition to modularizing for the purpose of handling the broad spectrum of vehicles, serious consideration had to be given to ease of reconfiguration in order to minimize test program turn around time.

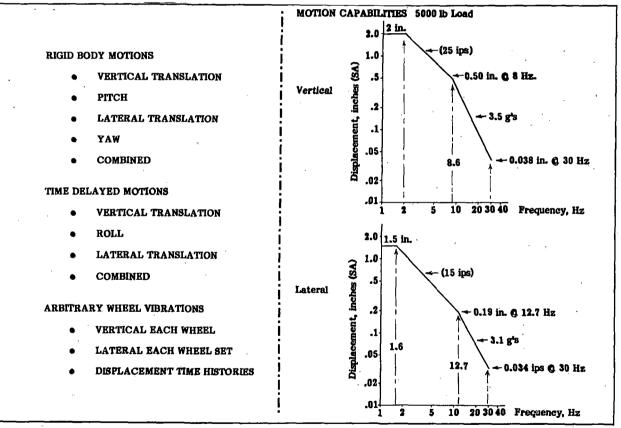


Fig. 5, VTU--Modes of Vibration

Requirements have been specified from (a) continuous VTU operation (periods up to 10 hours), (b) time required to start up/shutdown (four hours or less) and thereby permit a reasonable daily test period and (c) VTU configuration changes per test vehicle requirements (i.e., different truck axle spacings, etc.) in a reasonable time period. In addition, system safety requirements have been specified to prevent the VTU from damaging itself, the test An artist's rendering of one end of the VTU as designed and currently under construction and assembly at the RDL is presented in Figure 6. The VTU hardware as partially shown consists of the following major subsystems:

> Vertical excitation modules (one for each test vehicle wheel)

° Lateral excitation modules (one for each

test vehicle axle).

- Vehicle restraint mechanism (one for each coupler)
- Support elements such as reaction masses and service structures
- Hydraulic pumping and distribution system
- ^o Hybrid control and monitor system

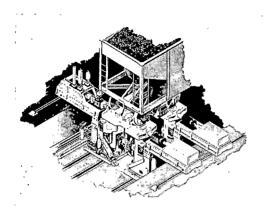


Fig. 6, Vibration Test Unit

The vertical excitation modules (each under independent servo control) are designed around a 60,000 lb (27,216 kg) hydraulic actuator, high performance servo-valve. Part of the actuator assembly is an air/oil biasing system designed to support the particular wheel load being tested such that the degradation of actuator dynamic force capability is minimal. The vertical moving elements are constrained to move in a vertical plane by three hydrostatically lubricated journal bearing designed to carry the attendant transverse forces during operation.

The lateral excitation modules (again each under independent servo control) are the most complicated of the VTU hardware elements in that the following parameters had to be accounted for:

- ^o Lateral translation (per axle basis)
- Lateral translation with a phase shift (per truck basis)
- Allowance for out of phase vertical motion (i.e., roll)
- Provision for longitudinal vehicle expansion and contraction as experienced during excitation of the lower body bending modes
- Minimum impact on truck polar moment of inertia
- ° Allowance for wheel lift-off

The combination of constraints, high instantaneous loads and overall performance demands resulted in a hardware configuration illustrated in more detail in Figure 7. The lateral excitation modules are centered around a 45,000 lb. (20,412 kg)₃ actuator assembly equipped with a 70 gpm (.0044m /s) high performance servo valve. In this case, oil/air biasing is provided on both sides of the primary moving elements in order to "sandwich" or preload the entire assembly. This approach was taken in order to provide minimum moving weight and roll moment of inertial of the moving elements. The motion capabilities of this subsystem as governed by the overall motion requirements previously identified are summarized below:

 $\Delta_{A} (In): + 1.78/ - 2.04 (+4.52/-5.18)*$ $\Delta_{B} (In): \pm 2.0 (\pm 5.08)*$ $\Delta_{C} (In): \pm 3.84 (\pm 9.75)*$ $\Delta_{P} (In): \pm 0.81 (\pm 2.06)*$ $\Theta_{P} (Deg): \pm 6.78(\pm .118)**$ $\Theta_{R} (Deg): \pm 3.85 (\pm .067)**$ $*() Cm_{**} () Cm_{Rad}$

The vehicle restraint mechanism is designed to limit the longitudinal rigid body motion of the test car and minimize spurious forces on the excitation modules. The device consists of a universal coupler adaptor, cable and preloading mechanism, with force measuring capabilities.

The support elements such as reaction masses and service structures are designed as permanent or moveable elements as appropriate to react vibratory loads and provide access as required for the variety of test configurations.

The hydraulic flow demands of the various excitation modules and hydrostatic bearing elements at peak excitation levels can be as high as 1,000 gpm ($.0631m^3/s$) @ 3,000 psi ($20,684,271N/m^2$) variable volume pumping systems each capable of delivering the rated flow at 3,000 psi (20,684, $271N/m^2$). The distribution manifolds provided allow for connection of the excitation modules in the required combinations of axles spacing and truck center distance.

The hybrid control and monitor system will permit the operation of the VTU from the remotely located control room of the RDL. The control consoles provide the approximate devices and displays for operation of the VTU in either a manual or automatic mode. This system consists of two major subsystems. A digital computer subsystem which will provide synthesized signals representing the "track environment" to the analog control and monitor subsystem in the automatic mode.

Portions of this control and monitor system

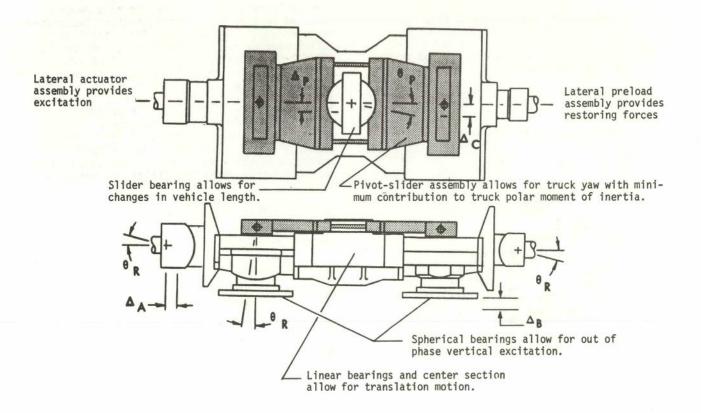


Fig. 7, VTU - Motion Capabilities

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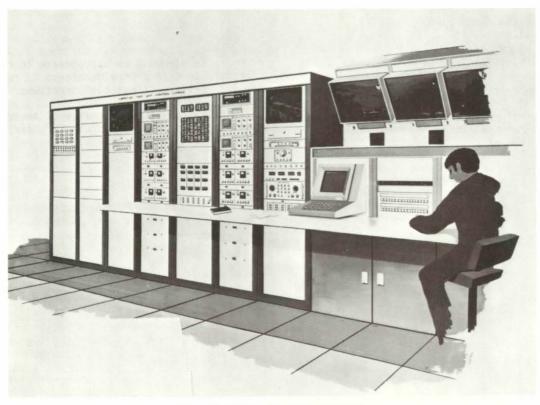


Fig. 8, VTU - Control Console

are shown in Figure 8. The complete analog control and monitor subsystem is illustrated as well as the master computer operations station.

RDU PERFORMANCE REQUIREMENTS

A brief summary of the major RDU performance requirements are noted here. Table 1 identifies the test vehicle weight and size limitations for the RDU, which is essentially the same as the former RDS requirements. Vehicle speed simulations are specified at 3-288 mph (4.8-463km/h) for up to 50,000 lb (22680 kg) axle load and 3-144 mph (4.8-232 km/ h) for 50,000 to 100,000 lbs (22680 kg to 45,360 kg) axle loads with special tolerance determined by GFP (drive train) capabilities. Likewise, simulation of wheel/rail traction forces have been specified but will be largely determined by modified GFP (drive train) capabilities.

In addition to driving both ends of the two-axle per truck vehicle, or one end of a three or four axle per truck vehicle, the RDU is required to have the capability to simulate steady state curve track operation (minimum curve radius) as follows:

a). 100 ft. (30.5m) for truck center of 50 ft. (15.2m) or less

b). 150 ft. (45.7m) for truck center between 50 and 80 ft (15.2 and 24.4m).

Requirements have been specified for reasonable times to reconfigure the RDU such as changing gage or axle spacing between rollers, or test vehicles of different length or different curve-radius track. Identical start up/ shutdown requirements (four hours or less) have been specified for the RDU as the VTU. During test operation, the RDU operator is only capable of increasing or decreasing the operator speed by manual adjustments. System safety requirements have been specified to prevent the RDU from damaging itself, the test vehicle or causing any hazard to operating/maintenance personnel. The RDU design capabilities have also been specified for the following future installations:

a) Body (lateral and roll) exciters to assess the effect of vehicle dynamic motion and forward speeds, b) installation of equipment for static loading to simulate the effect of super elevation unbalance during steady curve negotiations and c) automatic control of the RDU.

RDU HARDWARE CONFIGURATION

Like the VTU, the RDU hardware had to be designed to provide the capability to subject a variety of rail vehicles to dynamic tests, necessitating a modular hardware approach. The RDU, as shown in Figure 9, will support and drive (or absorb power from) the wheelsets of a four axle rail vehicle or a three or four axle locomotive truck. The rotation of the rollers will simulate vehicle speed on tangent track, and make possible the investigation of those phenomena which are independent of track irregularities, such as hunting modes. The RDU can also be configured to simulate steady state curve negotiations on tangent track.

The RDU consists of the following major subsystems:

- ° Drive trains
- ° Roller module units
- RDU support structures, reaction masses and structures
- ° Vehicle restraint system
- Service structures
- ° Control and monitor system

Each of the four drive trains is powered by a 600 hp (447.6 kw) variable speed motor. There is a master control station for synchronous operation of selected drive trains.

The roller module units (RMU), each driven by a drive train, will be equipped with two interchangeable sets of rollers, one set with a 42 in. (1.07 m) dia, and a second set with a 60 in. (1.52 m) dia. The smaller set will be used for simulation of vehicle speeds up to 144 mph (231.7 kmph) for axle loads under 100,000 lb (45,360 kg).

Each of the two RDU support structures (RDUSS) supports two drive trains and two RMUs. The RDUSS is equipped with air bearings to permit relocation of the RDUSS for various truck center distances and rotation to provide for simulated curves of up to 100 ft (30.48 m) in radius.

The vehicle restraint system controls the longitudinal position of the test vehicle, with respect to the RDU. This system consists of a cable, a flexibility element, a preloading device and a load measuring device. A reaction mass and structure are provided at each end of the test vehicle to react the loads generated by the vehicle, and transmitted through the vehicle restraint system.

Service structures consist of platforms, stairways and ladders required to provide access to and around the drive trains, roller module units, vehicle restraint systems, and test vehicle.

The control and monitor system will permit operations of the RDU from consoles located in the RDL control room. Speed of drive train rotation is commanded via a thumbwheel switch. Operational parameters are monitored and interlocked to prevent damage to the RDU or the test vehicle. The entire RDU control and monitor console is shown in Figure 10.

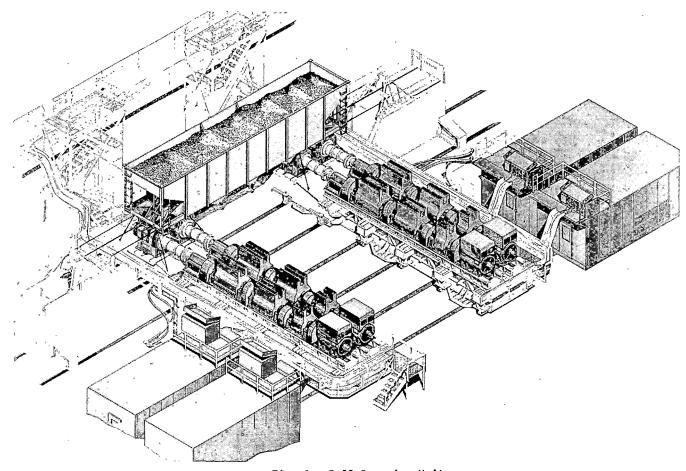


Fig. 9, Roll Dynamics Unit

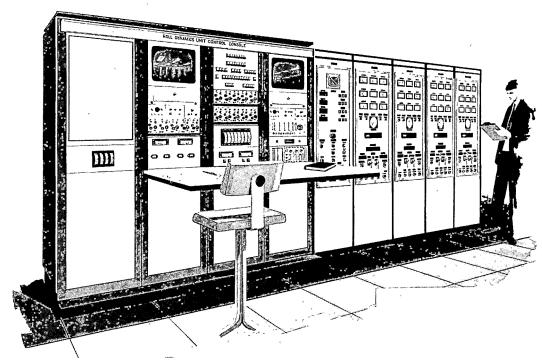


Fig. 10, RDU - Control Console

SPECIMEN DATA ACQUISITION SYSTEM (SDAS)

The VTU and RDU each have requirement for necessary data collection as implemented by SDAS. Figure 11 is a general description schematic of the SDAS. Additional data acquisition equipment as follows are available at TTC: (1) Calibration scanner, (2) photo motion analyzer, (3) closed circuit television, (4) video recording capability and (5) acoustic recording and analyzing capability. vehicles and advanced track systems under computer controlled conditions. Lessons learned in the RDL should lead to safer and lower cost equipment before it is built, not after mistakes are demonstrated in the field.

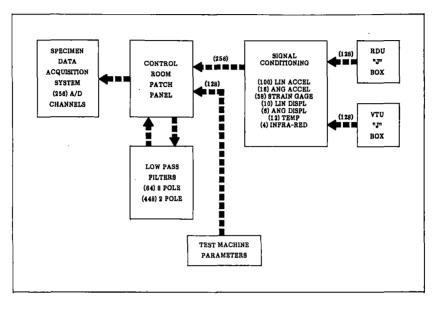


Fig. 11, SDAS General Description

VTU/RDU SYSTEM ACCEPTANCE TESTS

Acceptance tests for both the VTU and RDU are currently scheduled for late spring 1978. During these tests, Wyle Laboratories, the RDL contractor, will demonstrate that the performance requirements per contract statement-ofwork have been met. During this same time span training of TTC personnel to operate and maintain the VTU and RDU will be conducted.

SUMMARY

This paper has presented an overview of the RDL's VTU and RDU performance requirements and hardware configuration. At the time of preparing this paper a large percentage of the VTU and RDU designs were complete and fabrication under way. It is also noted, that when the RDL program was redirected via the DOT Task Force a finite budget was also imposed. Depending on the final program costs, the final VTU and RDU systems may be different than described in this paper. FRA is doing all that is fiscally possible to have the RDL facility operational as soon as possible: currently late spring or early summer 1978.

Once operational, the VTU and RDU will permit researchers to perform much needed analytical and experimental tests of full-scale locomotives, passenger and freight cars, transit

APPENDIX

Abstracts of Recent Reports and Magnetic Data Tapes Relating to Freight Systems R&D

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1.	Report No.	2. Government Access PB 252290	sion No.	3. Rec	ipient's Catalog No	•
4.	Title and Subtitle ANALYTICAL AND EXPERIMENTAL DETERM	INATION OF WHEEL-RAIL		5. Repo Dece	ort Date ember 30, 1975	
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7.	Authors N. K. Cooperrider, E. H. Law, R.	Hull, P. S. Kadala, J.	. M. Tuten	-8. Per	forming Organizatio	n Report No.
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4. Title and Subtitle			Report Date	
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7. Author's) Southern Pacific	Transportation	Company 8.	Performing Organization	on Report No:
Technical Research	n and Developme	nt Group	TDOP 75-251	
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16. Abstroct This document serves as a	n introduction	to the literature	e known to be	available
and relevant to rail frei	ght car trucks,	their components	s and performa	nce
characteristics. In conn	ection with the	Federal Railroad	l Administrati	on sponsored
research in Truck Design				
review and assemble all r documentation has been or			a articles.	ine collected
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• The History of the	Freight Car Tru	ick		
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Each section contains: a	n introduction	dealing with lite	erature select	ed for
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into three-volumes. Volu	me I contains t	the sections enti-	tled: "The Hi	story of the
Freight Car Truck" and "T	ruck Design."	Volumes II and II	II will comple	ete the
compilation. It is expec	ted that supple	ments to the thre	e initial vol	umes will
be published at a later d	ate as additior	al information be	ecomes availab	ole.
17. Key Words Bigliography, his	tory design	18. Distribution Statement		
principles, freight car tru		Document is avai		public
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Brakes and	Brake Rigging			
Centerplates	5			
• Side Frames	and Bolsters			
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7. Author's) Southern Pacific	Transportation Con	mpany	TDOP-75-153	
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4. Title and Subtitle		5.	Report Date	
FREIGHT CAR TRUCK DESIGN OP	TIMIZATION MET	HODOLOGY FOR	April , 1975	
A COMPREHENSIVE STUDY OF TR	JCK ECONOMICS	6.	Performing Organizatio	on Code
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7. Author's)		8.	Performing Organizatio	on Report No.
			TDOP 75-1	
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			. Work Unit No. (TRAI:	5)
Southern Pacific Tran One Market Street	spon cation C	ompany	. Contract or Grant No	*
San Francisco, Califo	mia 0/105		DOT FR-4002	
		13	. Type of Report and P	
12. Sponsoring Agency Name and Address				
U. S. Department of Th	ransportatio	n	Technical R	-January 1975
Federal Railroad Admin	istration	••	August 1974	-January 19/3
Office of Research, D		Demonstrat	n Sponsoring Agency C	ode
Washington, D. C. 209			· · · · ·	·
15. Supplementary Notes	- 		·····	
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16. Abstroct				•
Although TDOP centers testing specifications for evaluating the eco truck designs is not a to develop a systemati associated with truck developing the necessa study and subsequently the data from a wide b outline the findings o	for rail fr nomic benefit t hand. Acc c approach t ownership. ry truck ecc through the ase of source	reight car tru its to be deri cordingly, it h to identifying A methodology phomic data fi e collection a ces. A subsec	icks the meth ved from ef as been nec the cost e is propose is through and verifica	hodology ficient essary lements d for a pilot tion of
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19. Security Classif. (of this report)	20. Security Class	if. (of this page)	21. No. of Pages	22. Price
Unclassified	Unclassi		27	PC\$4.00 MF\$3.00

Form DOT F 1700.7 (8-72)

1. Report No.	2. Government Acce	ssion No. 3	. Recipient's Catalog	No.
	PB 25140	10		
FRA-OR&D 75-58A	PB 25140		. Report Date	
4. Title and Subtitle		TOTAL PROPERTY OF	March 1976	
FREIGHT CAR TRUCK DESIGN		6	March 1970 . Performing Organizat	ion Code
Truck Economic Data Colle	ection and Analy	vsis		
		8	. Performing Organizat	ion Report No.
7. Author's)				
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9. Performing Organization Name and Add	ress	Cash Name I	U. WORK UNIT NO. (TRA	15)
Southern Pacific Transpor	tation Company	1	1. Contract or Grant N	0.
One Market Street			DOT-FR-40023	
San Francisco, CA 94105		1	3. Type of Report and	Period Covered
12. Sponsoring Agency Name and Address			Technical Rep	
Department of Transportat	ion		Feb. 1975 - F	
Federal Railroad Administ	ration		160. 1979 - 1	20. 1970
Office of Research and De	evelopment	1	4. Sponsoring Agency	Code
Washington, D.C. 20590				
15. Supplementary Notes				
See also Freight Car Tr				
Study of Truck Economics,				
tent that this report exp	ands further on	the economic an	alysis of frei	ght car trucks
A first interim repo	ort covering the	development of	the TDOP econo	mic
methodology was published				
It contains the truck inv	vestment economi	c evaluation pro	cedures intend	ed for the
use of the railroad indus		-		
The primary objectiv	e of the Truck	Economic Data Co	llection and A	nalysis
Program is to test the pr	ocedures for es	tablishing the s	ignificant act	ual operating
costs of existing Type I	general purpose	trucks. This s	econd interim	report
covers the progress of th	e program. A g	eneralized truck	cost informat	ion system
was designed for the coll	ection and inte	gration of truck	economic data	. The
collection of test data f	or off-line tru	ck maintenance c	osts was compl	eted. Test
data collection was initi	ated for on-lin	e truck maintena	nce and other	associated
costs and operating condi				
appropriate data analysis	-	-		
data clearly revealed the	truck's report	ed off-line wear	and failure c	ost
performance.				
Railroad companies a		and the second s		-
the tested procedures of			11.11	
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a truck economic evaluati	on capability o	r their own.		
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19. Security Classif. (of this report)	20. Security Clas	sif. (of this page)	21. No. of Pages	22. Price
Unclassified	1	sified	86	PC\$5.00
				MF\$3.00

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1. Report No.	2. Government Acces	sion No. 3. F	Recipient's Catalog No.
FRA/ORD-76/287.I	PB 25936	56	
4. Title and Subtitle	,	5. F	eport Date
FREIGHT CAR TRUCK DESIGN OPT	TMT ZATTON		uly 1976
Economic Analysis Report -		6. F	erforming Organization Code
7. Author's) Couthorn Decific Tr			erforming Organization Repo rt No.
Technical Research & Develop	ment Group	1	DOP 76-3
9. Performing Organization Name and Addres		10.	Work Unit No. (TRAIS)
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San Francisco, California	4105		OT-FR-40023
	1200	13.	Type of Report and Period Covered
12. Sponsoring Agency Name and Address			achaigal Depart
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Federal Railroad Administrat			Sponsoring Agency Code
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<u>Washington, D.C.</u> 20590 15. Supplementary Notes See also: I	RA-ORED 75-58	. April 1975 (NTI	S Accession Number
PB 248 832) Methodology for	a Comprehensi	ve Study of Truck	Economics, and FRA
OR&D 75-58A, February 1976	NTIS Accessio	n Number PB 251 40	0) Truck Économic
Data Collection and Analysis		<u>·</u>	
16. Abstract This report summar	izes the truc	k economic researc	h accomplished during
Phase I of the Federal Rail			
Optimization Project (TDOP)			5
• A truck economic met	hodology was	devèloped with the	cooperation of
representatives from	the railroad	industry and thei	r suppliers. The
methodology is for :			
of the individual ra		ting trucks and ev	aluate investments
in proposed truck in	provements.	dontified and proc	edures were developed
at various levels of			
overall truck cost			
			tablish the integrated
truck economic data			
^o Economic data analys	sis guidelines	were developed to	establish and evaluate
the cash flows of in	nvestments in	proposed improveme	nts to existing trucks.
The approach to eva	uating the op	erating cost perfo	rmance of existing
trucks through the	exploitation of	of the economic dat	a base was developed.
The report recomme	ends that the	railroad industry	adapt the HOP
methodology developed thus begin to establish working	far to their	individual company	oction of existing
trucks and proposed improve	d truck desig	ms Suggested fur	ther economic
research is also identified		ins, buggested fur	
17. Key Words Freight Car Truck		18. Distribution Statement	able to the mublic
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Truck investment evaluation,		Virginia 22161	ee, chrangraora,
Car truck cash flow			
19. Security Classif. (of this report)	20. Security Clas	sif. (of this page)	21. No. of Pages 22. Price
Unclassified	Unclass	sified	PC\$4.50 MF\$3.00
01102000222200	1		μπ.φ.3.00

Form DOT F 1700.7 (8-72)

1. Report No.	2. Government Accessio	No. 3	Recipient's Catalog N	0
FRA-OR&D 76-05	PB 648633	1 C 12 2. 2. 3 3 4		
4. Title and Subtitle		5.	Report Date	
FREIGHT CAR TRUCK DESIGN	OPTIMIZATION		December 197	15
		6.	Performing Organizatio	on Code
Survey and Appraisal of T	ype II Trucks			
7. Author's) Southern Pacific	-	8.	Performing Organizatio	on Report No.
Souchern ractific	Transportation C	ompany	TDOD 75 001	
Technical Research 9. Performing Organization Name and Addre			TDOP 75-201	
		10.	Work Unit No. (TRAI	5)
Southern Pacific Transpor	tation Company	11	Contract or Grant No	
One Market Street			DOT-FR-40023	
San Francisco, California	94105	13.	Type of Report and P	lected Covered
12. Sponsoring Agency Name and Address				
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Washington, D.C. 20590	· - · · ·			
15. Supplementary Notes				
16. Abstract				
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tion's Truck Design Optim	ization Project.			
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